

Foot-mounted zerovelocity aided inertial navigation

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Course Outline

1. Foot-mounted inertial navigation

- a. Basic idea
- b. Pros and cons

2. Inertial navigation

- a. The inertial sensors
- b. The navigation equations
- c. Error propagation

3. Kalman filtering

- a. Direct filtering
- b. Complimentary filtering
- c. Pseudo observations and motion constraints

4. Zero-velocity detection

- a. Force sensitive resistors
- b. The SHOE detector
- c. Characteristics

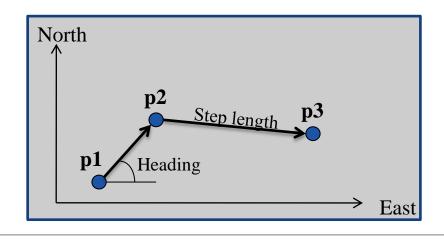
5. The OpenShoe project

- a. Background and Goal
- b. Hardware/Software
- c. Demo



Basic idea behind foot-mounted inertial navigation

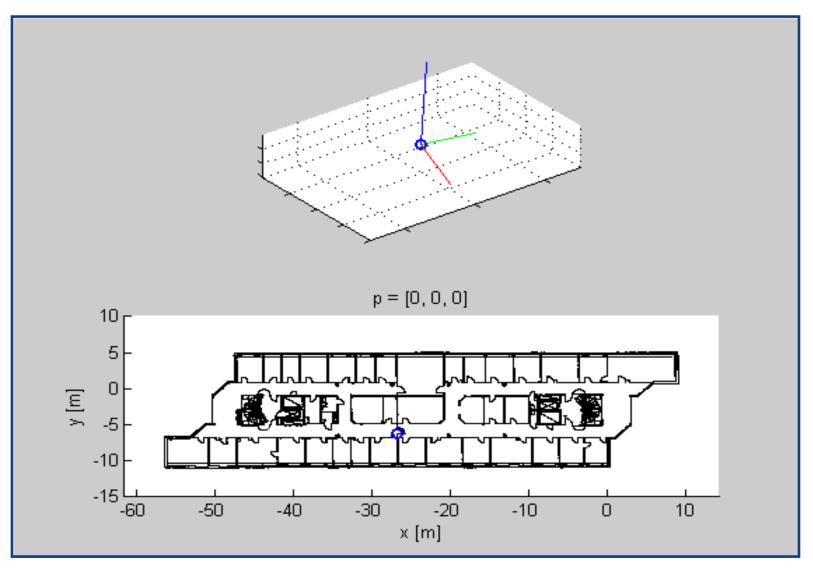
- 1. Mount (inertial) sensors in the sole of the shoes of a user
- 2. Measure the length and direction of the steps the users takes
- 3. Calculate the change in position via dead-reckoning.







Example: Output from a footmounted inertial navigation system





Pros and cons of foot-mounted inertial navigation

Pros

- Does not depend on any preinstalled infrastructure.
- Can not be disturbed.
- No motion constraints*.

Cons

- Initial position and heading most be known.
- The position and heading error grows with time.

^{*} We assume that the foot becomes stationary on a regular basis



Inertial navigation

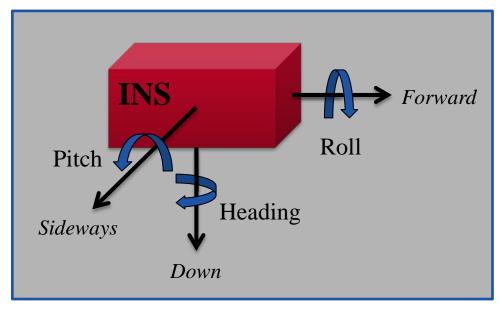
- Coordinate systems and rotations
- Sensors
- Navigation equations
- Error propagation

Notation

Description	Notation	
Discrete time index	k	
Sampling period	T_s	
Scalar	a	
Vector (matrix)	$\mathbf{a}\;(\mathbf{A})$	
Identity matrix	I	
Gravity vector	${f g}$	
Natural basis vector ℓ	\mathbf{e}_{ℓ}	
Transpose	$(\cdot)^T$	
Quantity expressed in coord. system j	$(\cdot)^j$	$j = \{e, n, b, i\}$
ℓ :th component of a vector	$[\mathbf{a}]_\ell$	
Rotation matrix	\mathbf{R}^n_b	
Cross product	$\mathbf{a} imes \mathbf{b}$	
Cross product matrix	$[\mathbf{a}]_{\times}$	$[\mathbf{a}]_ imes \mathbf{b} = \mathbf{a} imes \mathbf{b}$
Perturbation	$\delta {f a}$	
Estimated quantity	$\hat{\mathbf{a}}$	$\widehat{\mathbf{a}} = \mathbf{a} + \delta \mathbf{a} \widehat{\mathbf{R}}_b^n = (\mathbf{I} - [\epsilon]_{\times}) \mathbf{R}_b^n$
Measured quantity	$\widetilde{\mathbf{b}}$	$\widetilde{\mathbf{b}} = \mathbf{b} + \delta \mathbf{b}$



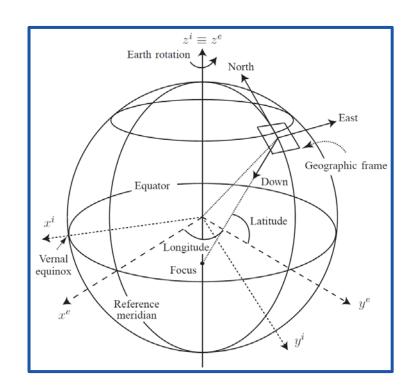
Coordinate systems and rotations



Body coordinate system and the three Euler angles.

Orientation representation

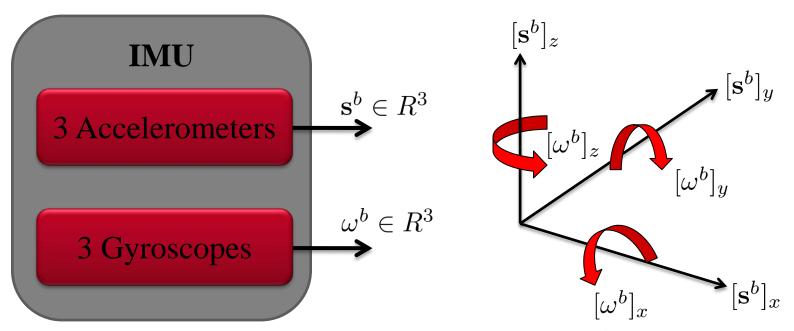
- Euler angles (roll, pitch, yaw) θ
- Roatation matrix \mathbf{R}_b^n , $\mathbf{a}^n = \mathbf{R}_b^n \mathbf{a}^b$
- Quaternion vector **q**



Earth centered inertial, earth centered earth fixed, and geographic coordinate system.



Inertial measurement unit (IMU)



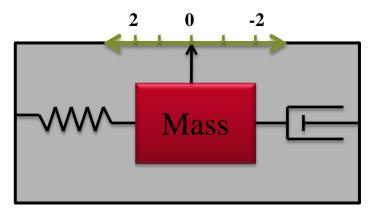
Body (or platform) coordinate system

Minimum requirements

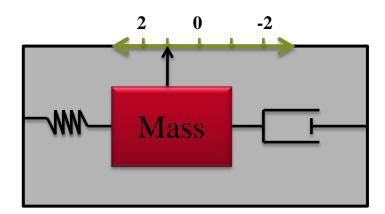
- Sampling rate 100 Hz
- \bullet Accelerometer dynamic range $\pm 15g$
- ullet Gyroscope dynamic range $\pm 1200^\circ/s$



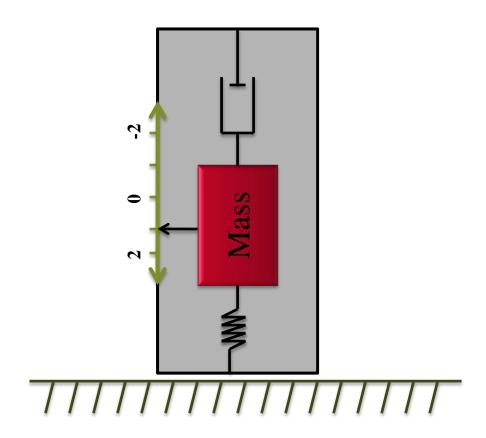
The accelerometer and its output (1)



Stationary accelerometer.



Accelerometer accelerating to the right, and with the sensitivity axis orthogonal to the gravity field.



Accelerometer stationary on the earth and with the sensitivity axis aligned with the gravity field.

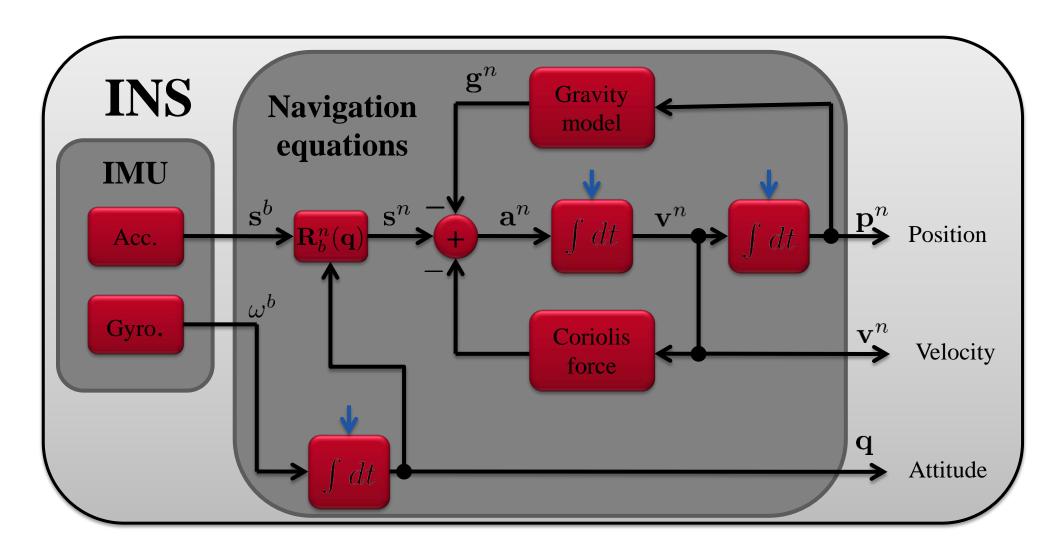


The accelerometer and its output (2)

- The inertial and gravitational acceleration are indistinguishable to a accelerometer.
- The output of an accelerometer is called *specific force*, and includes both the inertial acceleration and the gravity acceleration.
- To calculate the inertial acceleration from the specific force output of an IMU we most know the IMUs orientation w.r.t. the geographic coordinate system.



Inertial navigation system (INS)





The navigation equations

For a foot-mounted INS using low-cost sensors the following navigation equations can be used.

$$\mathbf{x}(k) = f\left(\mathbf{x}(k-1), \mathbf{s}^b(k), \omega^b(k)\right) \quad \mathbf{x}(0) = \{\text{Initial Condition}\}\$$
 where

$$\mathbf{x}(k) = \begin{bmatrix} (\mathbf{p}^n(k))^T & (\mathbf{v}^n(k))^T & (\mathbf{q}(k))^T \end{bmatrix}^T$$

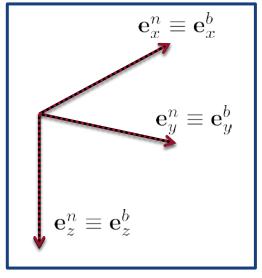
where
$$\mathbf{x}(k) = \begin{bmatrix} (\mathbf{p}^{n}(k))^{T} & (\mathbf{v}^{n}(k))^{T} & (\mathbf{q}(k))^{T} \end{bmatrix}^{T}$$

$$f: \begin{cases} \mathbf{p}^{n}(k) = \mathbf{p}^{n}(k-1) + T_{s}\mathbf{v}^{n}(k) \\ \mathbf{v}^{n}(k) = \mathbf{v}^{n}(k-1) + T_{s}\left(\mathbf{R}_{b}^{n}(\mathbf{q}(k))\mathbf{s}^{b}(k) - \mathbf{g}^{n}\right) \\ \mathbf{q}(k) = \left(\cos(\frac{T_{s}\|\omega^{b}(k)\|}{2})\mathbf{I} + \frac{2}{T_{s}\|\omega^{b}(k)\|}\sin(\frac{T_{s}\|\omega^{b}(k)\|}{2})\mathbf{\Omega}(k)\right)\mathbf{q}(k-1) \end{cases}$$

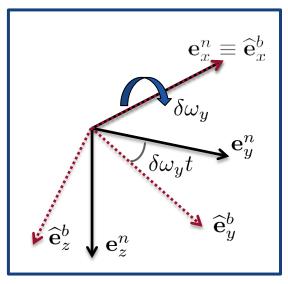
$$\mathbf{\Omega}(k) = \frac{T_s}{2} \begin{bmatrix} 0 & [\omega^b(k)]_z & -[\omega^b(k)]_y & [\omega^b(k)]_x \\ -[\omega^b(k)]_z & 0 & [\omega^b(k)]_x & [\omega^b(k)]_y \\ [\omega^b(k)]_y & -[\omega^b(k)]_x & 0 & [\omega^b(k)]_z \\ -[\omega^b(k)]_x & -[\omega^b(k)]_y & -[\omega^b(k)]_z & 0 \end{bmatrix}$$



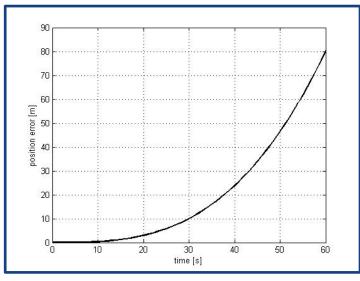
Error propagation



True orientation of the navigation and body coordinate system.



Orientation of the estimated body coordinate system after t [s].



Position error as a function of time with a gyroscope bias of 0.013 deg/s.

$$\delta \mathbf{a}^n = \mathbf{a}^n - \widehat{\mathbf{a}}^n = \mathbf{0} - (\widehat{\mathbf{R}}_b^n \mathbf{s}^b - \mathbf{g}^n) = \mathbf{g}^n - \widehat{\mathbf{R}}_b^n \mathbf{R}_n^b \mathbf{g}^n = \mathbf{g}^n - (\mathbf{I} - [\epsilon]_{\times}) \mathbf{R}_b^n \mathbf{R}_n^b \mathbf{g}^n = \begin{bmatrix} 0 \\ -g[\delta \omega]_y t \\ 0 \end{bmatrix}$$

$$\Rightarrow |[\delta \mathbf{p}^n(\tau)]_y| = |\int_0^\tau [\delta \mathbf{a}^n]_y dt| = \frac{|[\delta \omega^b]_y|g\tau^3}{6}$$

Error state space model

The error in the foot-mounted INS can be modeled as

$$\delta \mathbf{x}(k) = \mathbf{F}(k)\delta \mathbf{x}(k-1) + \mathbf{G}(k)\mathbf{w}(k)$$

$$\delta \mathbf{x}(k) = \begin{bmatrix} (\delta \mathbf{p}^n(k))^T & (\delta \mathbf{v}^n(k))^T & (\epsilon(k))^T \end{bmatrix}^T$$

The error in the root-mounted TVS can be modeled as
$$\delta \mathbf{x}(k) = \mathbf{F}(k)\delta \mathbf{x}(k-1) + \mathbf{G}(k)\mathbf{w}(k)$$
 where
$$\delta \mathbf{x}(k) = \begin{bmatrix} (\delta \mathbf{p}^n(k))^T & (\delta \mathbf{v}^n(k))^T & (\epsilon(k))^T \end{bmatrix}^T$$

$$\mathbf{F}(k) = \begin{bmatrix} \mathbf{I} & T_s \mathbf{I} & \mathbf{0} \\ \mathbf{0} & \mathbf{I} & T_s [\mathbf{s}^n(k)]_{\times} \\ \mathbf{0} & \mathbf{0} & \mathbf{I} \end{bmatrix} \quad \mathbf{G}(k) = \begin{bmatrix} \mathbf{0} & \mathbf{0} \\ \mathbf{R}_b^n(k) & \mathbf{0} \\ \mathbf{0} & \mathbf{R}_b^n(k) \end{bmatrix}$$

 $\mathbf{w}(k)$ - Additive white noise with covariance matrix \mathbf{Q}

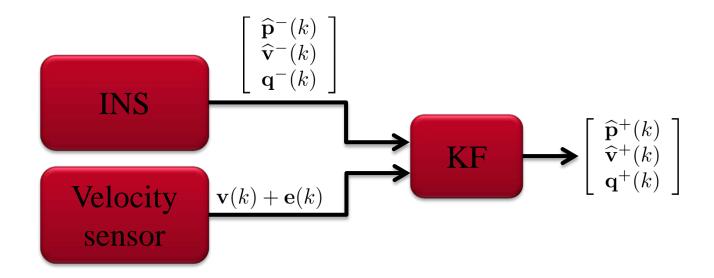
Note that
$$\mathbf{x}(k) = \Gamma(\widehat{\mathbf{x}}(k), \delta \mathbf{x}(k))$$
, where $\Gamma : \begin{cases} \mathbf{p}^{n}(k) = \widehat{\mathbf{p}}^{n}(k) + \delta \mathbf{p}^{n}(k) \\ \mathbf{v}^{n}(k) = \widehat{\mathbf{v}}^{n}(k) + \delta \mathbf{v}^{n}(k) \\ \mathbf{q}(k) = h_{\mathbf{R}}^{\mathbf{q}} \left((\mathbf{I} + [\epsilon(k)]_{\times}) \mathbf{R}_{b}^{n}(\widehat{\mathbf{q}}(k)) \right) \end{cases}$



Kalman filtering and INSs

- Direct filtering
- Complementary filtering
- Feedback structure
- Pseudo observations and motion constraints

Direct filtering



Pros

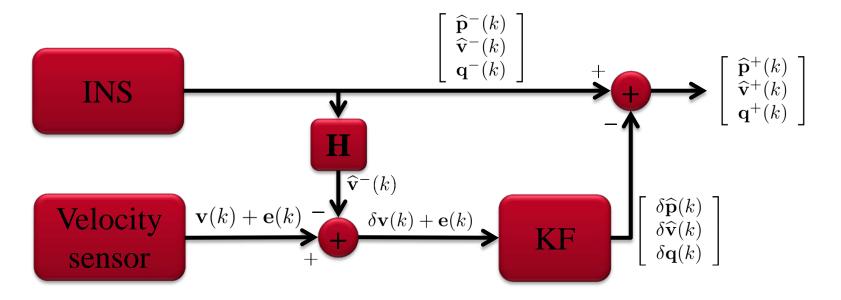
• Simple filter structure.

Cons

- It is difficult to model the motion dynamics in the KF framework.
- High computational load due to the high update rate of the INS.



Complementary filtering (feedforward)



Pros

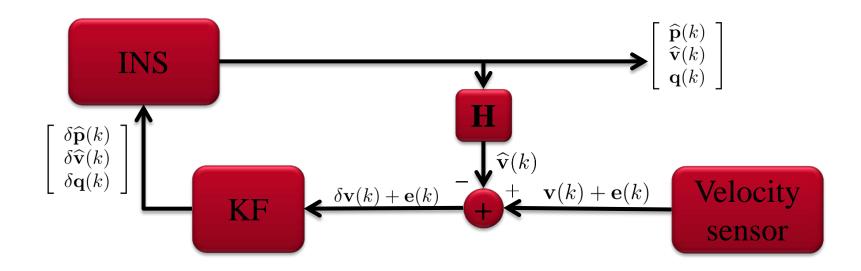
- The KF estimates the navigation state errors, which can be better modeled in the KF framework.
- The KF needs only to be updated at the sample rate of the velocity sensor.

Cons

Numerical problems with low-cost INS.



Complementary filtering (feedback)



Pros

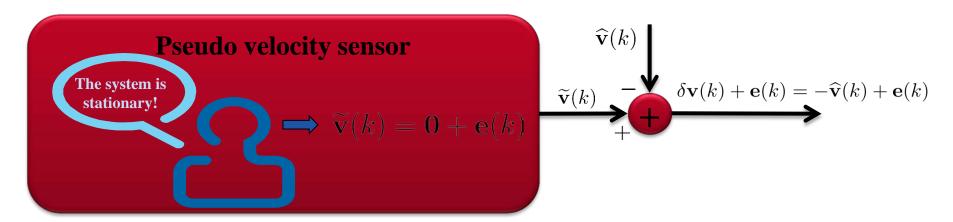
- The KF estimates the navigation state errors, which can be better modeled in the KF framework.
- The KF needs only to be updated at the sample rate of the velocity sensor.

Cons

• If something goes wrong in the error estimation, the navigation solution can be destroyed for all time.



Zero-velocity updates



The observation equations for the error state space model in a zero-velocity aided INS can be written as

$$\mathbf{y}(k) = \mathbf{H}(k) \, \delta \mathbf{x}(k) - \mathbf{e}(k)$$

where

$$\mathbf{y}(k) = -\mathbf{H}(k)\widehat{\mathbf{x}}(k)$$

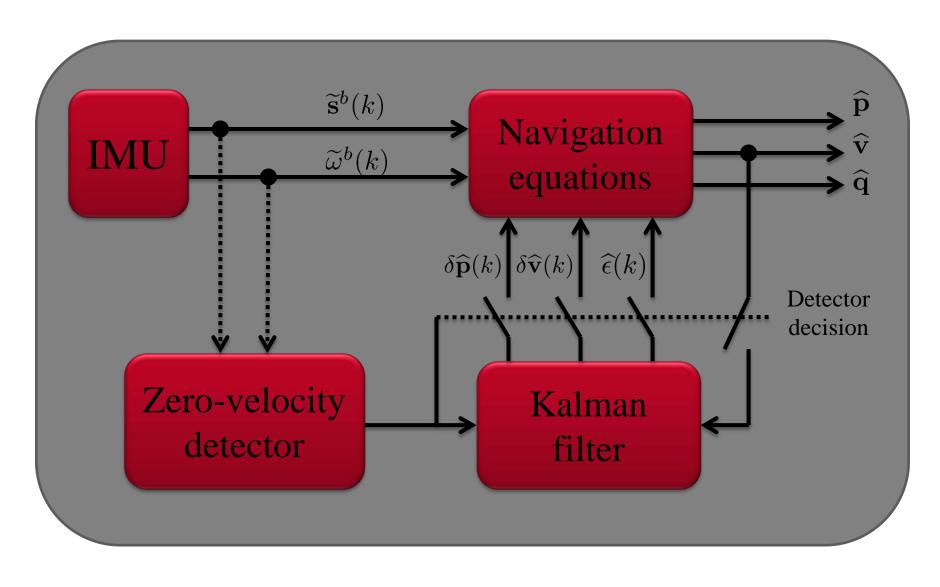
$$\mathbf{H}(k) = \begin{cases} \mathbf{H} & \text{System is stationary} \\ \mathbf{0}_{3,9}, & \text{Otherwise} \end{cases}$$

$$\mathbf{H} = \begin{bmatrix} \mathbf{0}_{3,3} & -\mathbf{I}_3 & \mathbf{0}_{3,3} \end{bmatrix}$$

 $\mathbf{e}(k)$ is additive white noise with covariance matrix \mathbf{R}



The zero-velocity aided INS Kalman filter structure.



Pseudo code for the KF based zerovelocity aided INS

```
\mathbf{P}(0) \leftarrow \mathbf{Process}\{\text{Initial state covariance matrix}\}\
\widehat{\mathbf{x}}(0) \leftarrow \mathbf{Process}\{\text{Initial navigation state}\}\
loop
     \widehat{\mathbf{x}}(k) \leftarrow f(\widehat{\mathbf{x}}(k-1), \widetilde{\mathbf{s}}(k), \widetilde{\omega}(k))
     \mathbf{P}(k) \leftarrow \mathbf{F}(k) \mathbf{P}(k-1) \mathbf{F}^T(k) + \mathbf{G}(k) \mathbf{Q} \mathbf{G}^T(k)
     T(k) \leftarrow \mathbf{Process}\{\text{Zero-velocity detector}\}\
     if T(k) \leq \gamma then
           \mathbf{y}(k) \leftarrow -\mathbf{H}\widehat{\mathbf{x}}(k)
           \mathbf{K} \leftarrow \mathbf{P}(k) \mathbf{H}^T (\mathbf{H} \mathbf{P}(k) \mathbf{H}^T + \mathbf{R})^{-1}
           \delta \widehat{\mathbf{x}}(k) \leftarrow \mathbf{K}\mathbf{y}(k)
           \widehat{\mathbf{x}}(k) \leftarrow \Gamma(\widehat{\mathbf{x}}(k), \delta\widehat{\mathbf{x}}(k))
           \mathbf{P}(k) \leftarrow (\mathbf{I} - \mathbf{K} \mathbf{H}) \mathbf{P}(k)
           k \leftarrow k+1
      end if
end loop
```

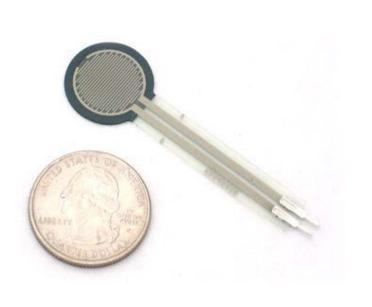


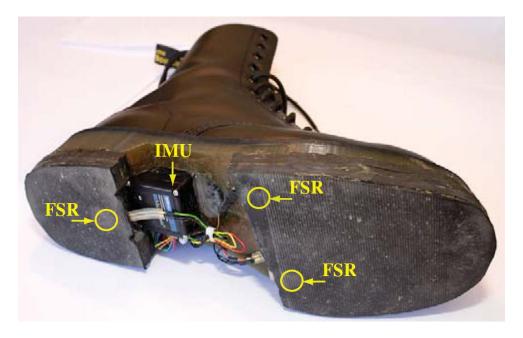
Zero-velocity detection

- Force sensitive resistors as a detector
- Zero-velocity detection using IMU data
- The SHOE detector



Force sensitive resistors (FSR) as zero-velocity detector



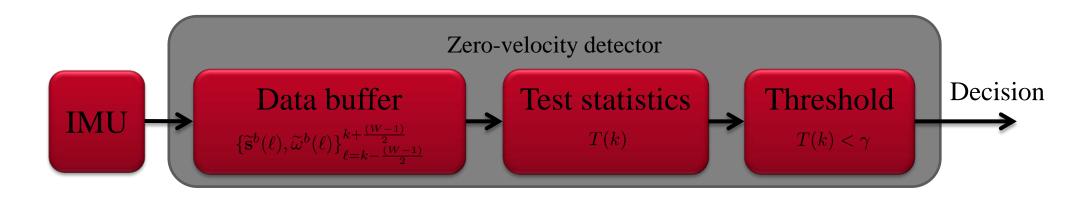


Drawbacks

- Sensitive to mechanical fatigue
- Threshold is weight dependent
- Only works when pressure is applied



Zero-velocity detection using IMU data



When the system is stationary, then

- The specific force measured by the accelerometers is equal to the gravitation acceleration, whose magnitude is known.
- The attitude of the IMU is constant, i.e., the angular rate experienced by the IMU is zero.

The SHOE detector



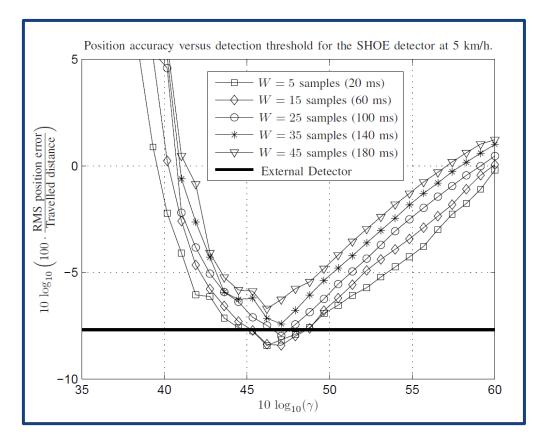
$$T(k) = \frac{1}{W} \sum_{\ell=k-\frac{W-1}{2}}^{k-\frac{W-1}{2}} \left(\frac{1}{\sigma_a^2} \| \widetilde{\mathbf{s}}^b(\ell) - g \frac{\overline{\mathbf{s}}(k)}{\| \overline{\mathbf{s}}(k) \|} \|^2 + \frac{1}{\sigma_\omega^2} \| \widetilde{\omega}(\ell) \|^2 \right)$$

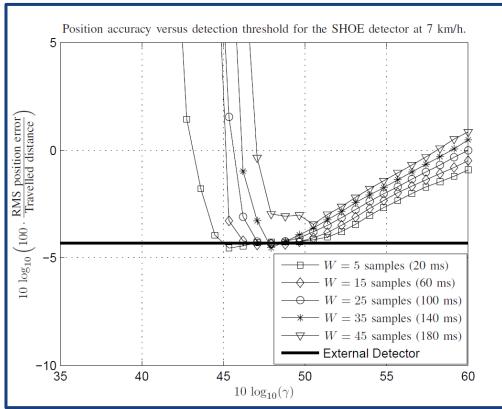
where

$$\overline{\mathbf{s}}(k) = \frac{1}{W} \sum_{\ell=k-\frac{W-1}{2}}^{k-\frac{W-1}{2}} \widetilde{\mathbf{s}}^b(\ell)$$



Position error as a function of the detector settings.





Conclusions

- SNR is high \rightarrow Keep the window size W small to get a fast detector.
- The "optimal" threshold γ varies little with the gait speed.



The OpenShoe project

- Introduction
- Hardware
- Software
- Demo



OpenShoe – Foot-mounted INS for Every Foot



www.openshoe.org

 OpenShoe is an open source embedded foot-mounted INS implementation including both hardware and software design.

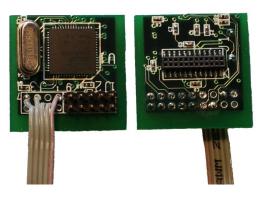


Hardware

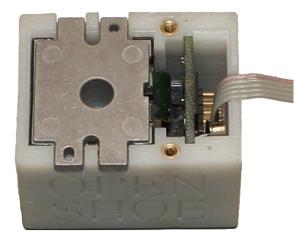


IMU





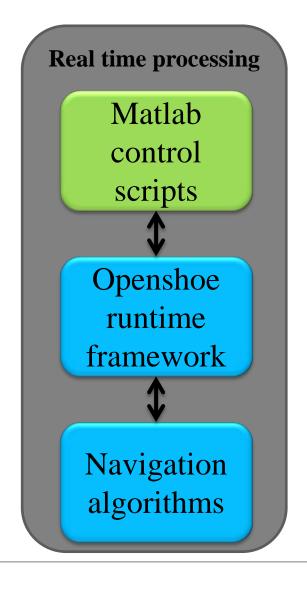
Microcontroller board

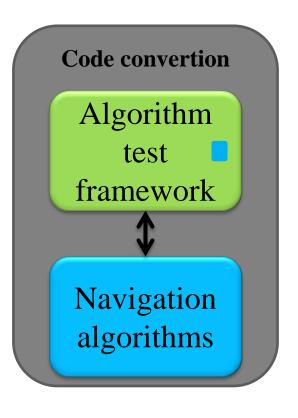


Embedded system



Software





Matlab scripts

Algorithm testing Openshoe Matlab Toolbox C code running on the microcontroller